

Algebraic Multigrid Techniques for the eXtended Finite Element Method

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Thanks to: E. Boman, J. Gaidamour (Sandia),
B. Hiriyyur, H. Waisman (Columbia U.)

- Overview & Motivation
 - A brief review of XFEM
 - Why does standard SA-AMG fail & how to fix it
 - Examples
 - Conclusion



Sandia is a multiprogram laboratory managed and operated by Sandia Corporation, a Lockheed Martin Company, for the United States Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.

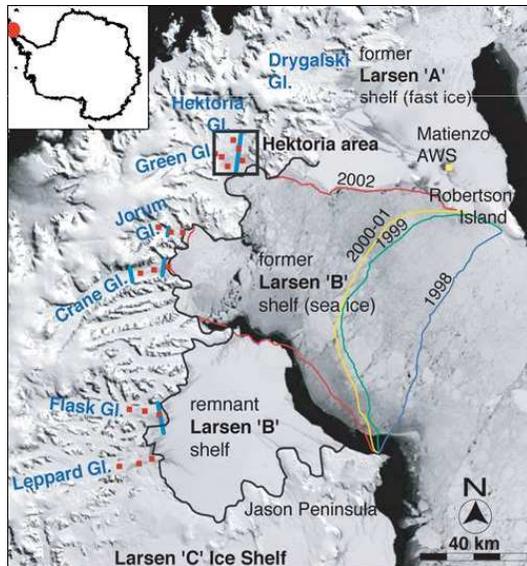


Fracture of ice

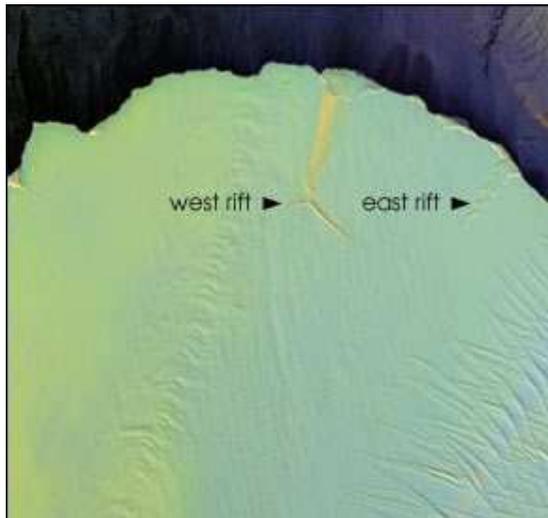
Objective: Employ parallel computers to better understand how fracture of land ice affects the global climate. Fracture happens e.g. during

- the collapse of ice shelves,
- the calving of large icebergs, and
- the role of fracture in the delivery of water to the bed of ice sheets.

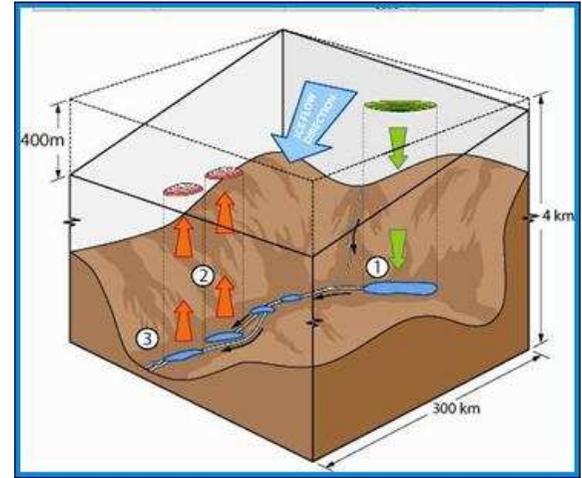
Ice shelves in Antarctica:



Larsen 'B' diminishing shelf
1998-2002
Other example: Wilkins ice shelf 2008



Amery ice shelf



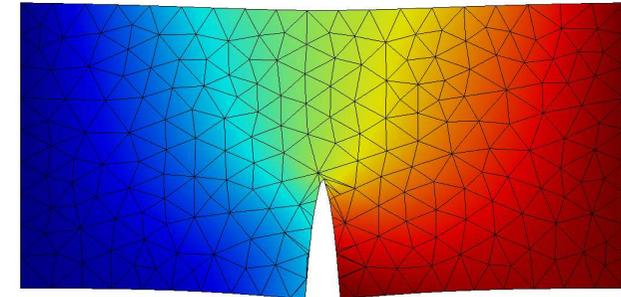
Glacial hydrology
(Source: <http://www.sale.scar.org>)



Computational Modeling of Fracture

Classical FEM approach to fracture mechanics

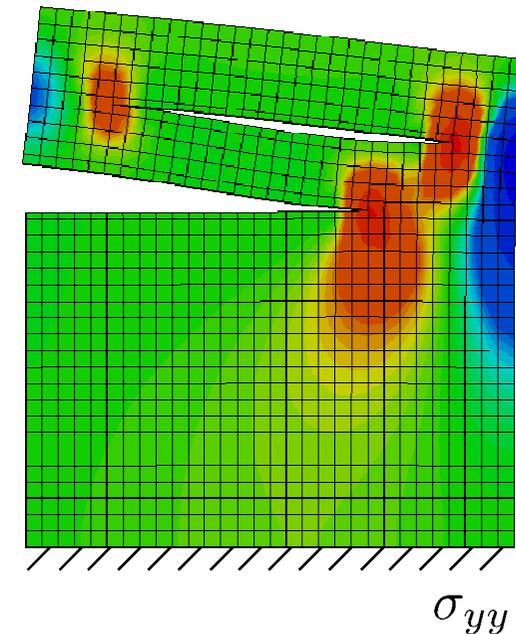
- Mesh conforms to crack boundaries
- Crack propagation \rightarrow remeshing at each step
 - Requires fine mesh for tip singularities
 - Mesh smoothing for 'ugly' elements



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eXtended Finite Element Method (XFEM)*

- Base mesh independent of crack geometry
- Crack propagation \rightarrow adding "enriched" DOF with special basis functions to existing nodes
 - Number of DOFs change, mesh does not



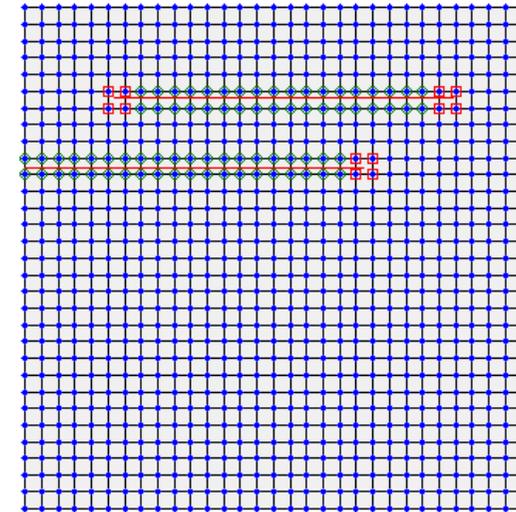
* Belytschko & Black (1999), Moës et al. (1999)



XFEM Formulation for Cracks

Displacement approximation (shifted basis form.)

$$\begin{aligned}
 u^h(\mathbf{x}) &= \sum_{I=1}^n N_I(\mathbf{x}) u_I \\
 &\quad \blacksquare + \sum_{i=1}^{n_h} N_{I_i}(\mathbf{x}) (H(\mathbf{x}) - H(\mathbf{x}_{I_i})) a_{I_i} \\
 &\quad \blacksquare + \sum_{i=1}^{n_f} N_{\hat{I}_i}(\mathbf{x}) \sum_{J=1}^{n_J} (F_J(\mathbf{x}) - F_J(\mathbf{x}_{\hat{I}_i})) b_{\hat{I}_i J}
 \end{aligned}$$



■ Jump Enrichment

$$H(\mathbf{x}) = \begin{cases} 0.5 & \text{in } \Omega^+ \\ -0.5 & \text{in } \Omega^- \end{cases}$$

■ Tip Enrichment (brittle crack)

$$F_J(r, \theta) = \left\{ \overbrace{\sqrt{r} \sin\left(\frac{\theta}{2}\right)}^{J=1}, \overbrace{\sqrt{r} \cos\left(\frac{\theta}{2}\right)}^{J=2}, \overbrace{\sqrt{r} \sin\left(\frac{\theta}{2}\right) \sin(\theta)}^{J=3}, \overbrace{\sqrt{r} \cos\left(\frac{\theta}{2}\right) \sin(\theta)}^{J=4} \right\}$$

Bubnov-Galerkin method: use identical approximation for test function $\delta \mathbf{d}(\mathbf{x})$

→ Symmetric global system

$$\mathbf{A} = \sum_e \int_{\Omega_e} \mathbf{B}_e^T \mathbf{C} \mathbf{B}_e \, d\mathbf{x}$$

$$\mathbf{f} = \sum_e \int_{\Gamma_e} \mathbf{N}_e^T h \, d\mathbf{x} + \sum_e \int_{\Omega_e} \mathbf{N}_e^T \rho \, d\mathbf{x}$$

$$\mathbf{A} \mathbf{u} = \mathbf{f}$$

Current implementation: bi-linear, Lagrange polynomials, quad4 elements



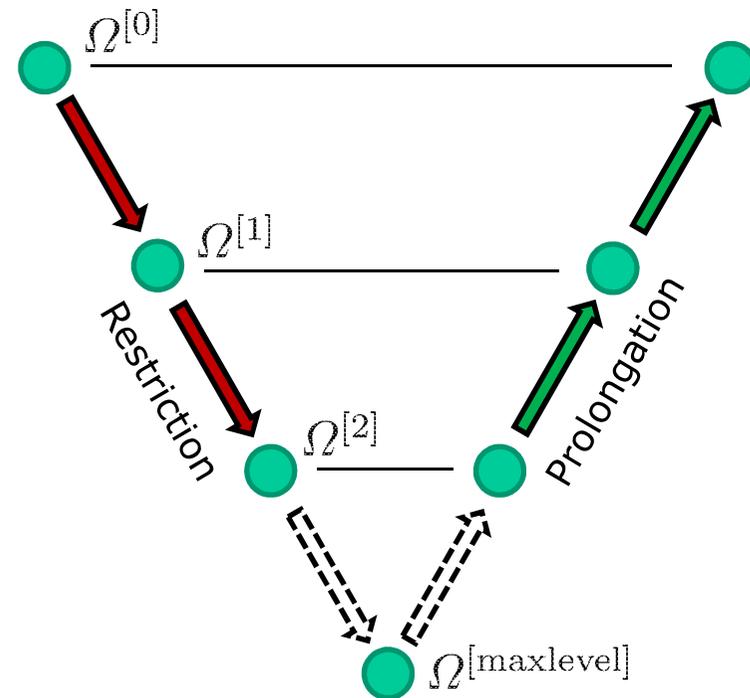
Multigrid principles

- Oscillatory components of error are reduced effectively by smoothing, but smooth components attenuate slower
- → capture error at multiple resolutions using grid transfer operators $R^{[k]}$ and $P^{[k]}$
- **In AMG**, transfer operators are obtained from **graph information of A**
- Interpolation complements relaxation

solve $Au=b$ using recursive multilevel V Cycle:

```

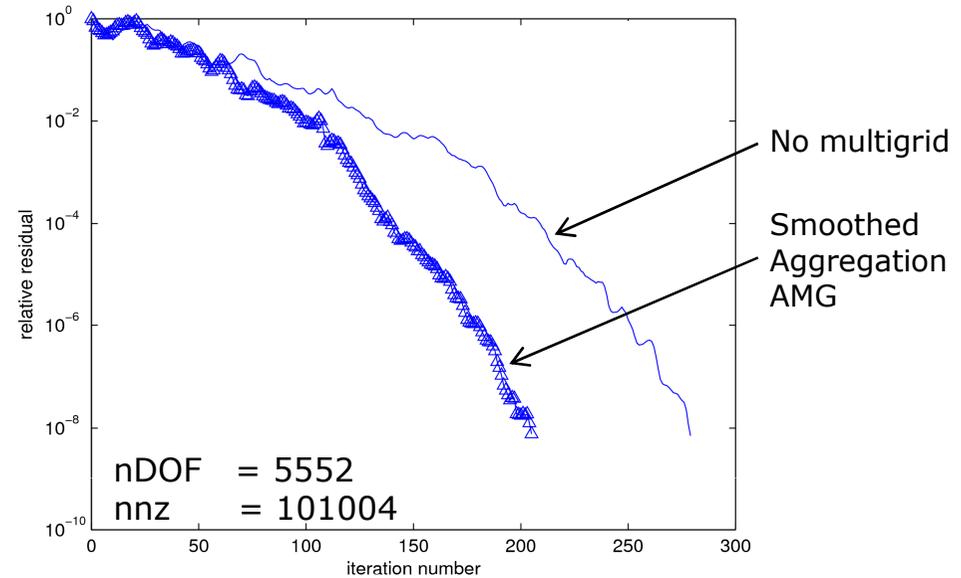
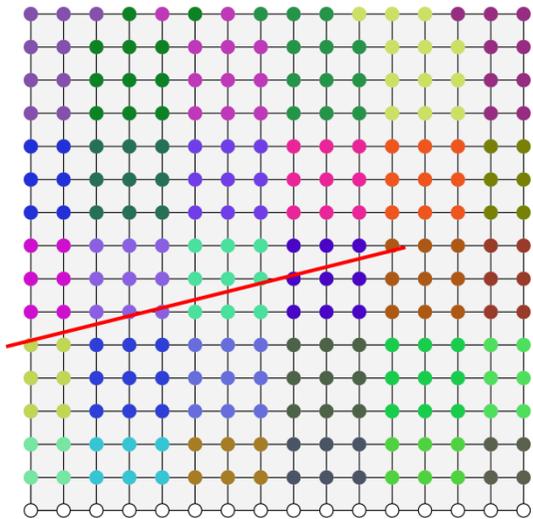
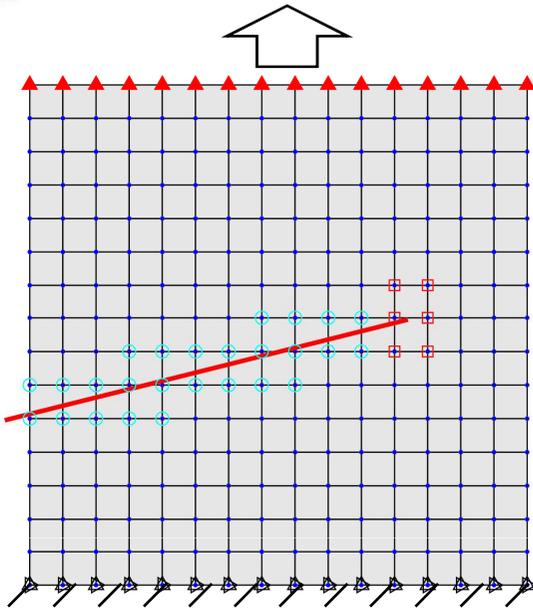
function  $u \leftarrow$  multilevel( $b, u, k$ )
 $u = S_{\text{PreSmoother}}^{[k]}(A^{[k]}, b, u)$ 
if  $k < \text{maxlevel}$  then
   $b_c = R^{[k]} \cdot (b - A^{[k]}u)$ 
   $u_c = \text{multilevel}(b_c, \mathbf{0}, k + 1)$ 
   $u = u + P^{[k]} \cdot u_c$ 
 $u = S_{\text{PostSmoother}}^{[k]}(A^{[k]}, b, u)$ 
return  $u$ 
  
```



- iterative smoother on finest and intermediate levels
- direct solve at the coarsest level



'Standard' SA-AMG for fracture problems

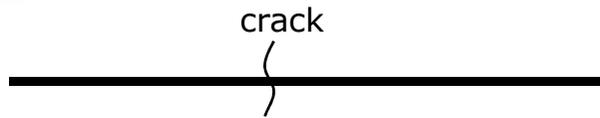


Possible issues:

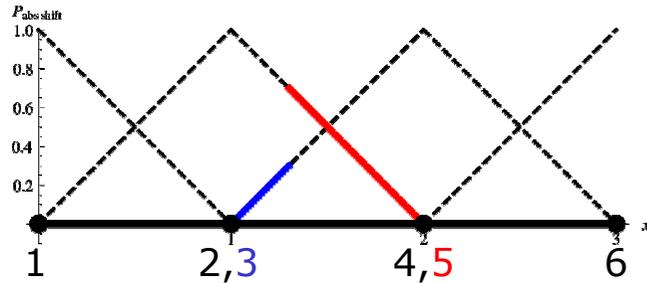
- Aggregation
 - Aggregates should not cross crack
- Nullspace
 - Elasticity: 3 ZEMs
 - Uncoupled domains: 6 ZEMs? or more?
- Assumption of 2 unknowns per node fails
 - 2, 4, or 10 DOFs per node



Distinct region representation



XFEM: modified shifted enrichment



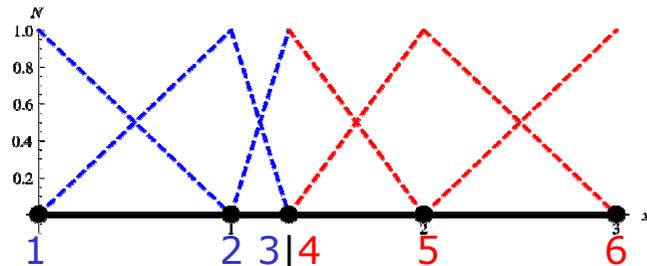
$$\sum_I N_I(x) |H(x) - H(x_I)| a_I$$

$$\frac{EA}{2h_1} \begin{bmatrix} 2 & -2 & 0 & 0 & 0 & 0 \\ -2 & 4 & 1 & -2 & -1 & 0 \\ 0 & 1 & 1 & -1 & 0 & 0 \\ 0 & -2 & -1 & 4 & 1 & -2 \\ 0 & -1 & 0 & 1 & 1 & 0 \\ 0 & 0 & 0 & -2 & 0 & 2 \end{bmatrix}$$

M

$$\frac{\rho Ah_1}{24} \begin{bmatrix} 8 & 4 & 0 & 0 & 0 & 0 \\ 4 & 16 & 1 & 4 & 2 & 0 \\ 0 & 1 & 1 & 2 & 0 & 0 \\ 0 & 4 & 2 & 16 & 1 & 4 \\ 0 & 2 & 0 & 1 & 1 & 0 \\ 0 & 0 & 0 & 4 & 0 & 8 \end{bmatrix}$$

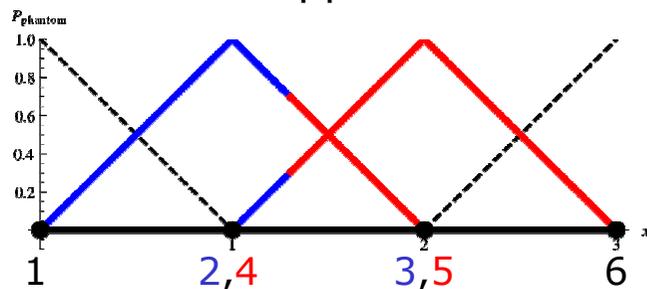
FEM



$$\frac{EA}{2h_1} \begin{bmatrix} 2 & -2 & 0 & 0 & 0 & 0 \\ -2 & 6 & -4 & 0 & 0 & 0 \\ 0 & -4 & 4 & 0 & 0 & 0 \\ 0 & 0 & 0 & 4 & -4 & 0 \\ 0 & 0 & 0 & -4 & 6 & -2 \\ 0 & 0 & 0 & 0 & -2 & 2 \end{bmatrix}$$

$$\frac{\rho Ah_1}{24} \begin{bmatrix} 8 & 4 & 0 & 0 & 0 & 0 \\ 4 & 12 & 2 & 0 & 0 & 0 \\ 0 & 2 & 4 & 0 & 0 & 0 \\ 0 & 0 & 0 & 4 & 2 & 0 \\ 0 & 0 & 0 & 2 & 12 & 4 \\ 0 & 0 & 0 & 0 & 4 & 8 \end{bmatrix}$$

Phantom node approach

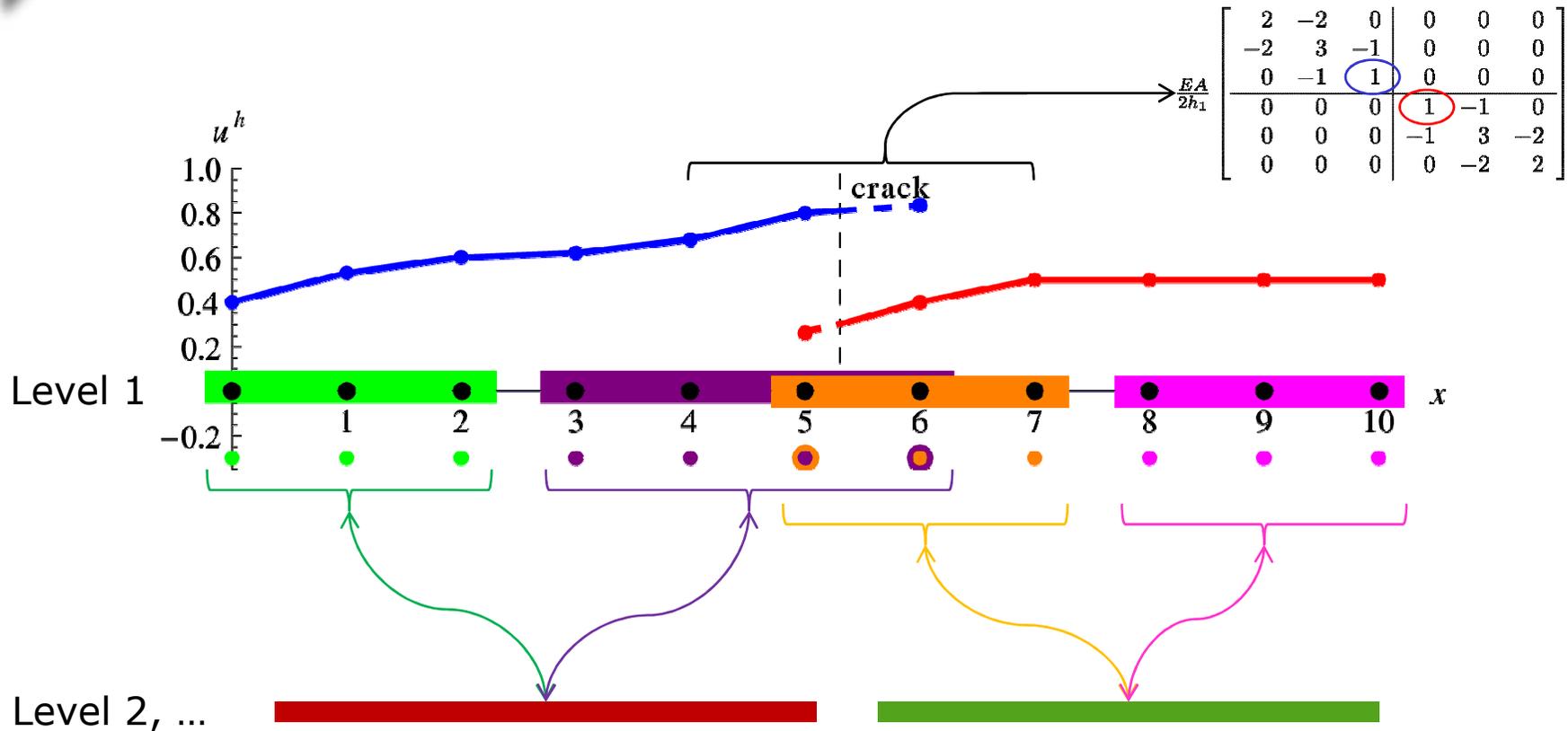


$$\frac{EA}{2h_1} \begin{bmatrix} 2 & -2 & 0 & 0 & 0 & 0 \\ -2 & 3 & -1 & 0 & 0 & 0 \\ 0 & -1 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & -1 & 0 \\ 0 & 0 & 0 & -1 & 3 & -2 \\ 0 & 0 & 0 & 0 & -2 & 2 \end{bmatrix}$$

$$\frac{\rho Ah_1}{24} \begin{bmatrix} 8 & 4 & 0 & 0 & 0 & 0 \\ 4 & 15 & 2 & 0 & 0 & 0 \\ 0 & 2 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 2 & 0 \\ 0 & 0 & 0 & 2 & 15 & 4 \\ 0 & 0 & 0 & 0 & 4 & 8 \end{bmatrix}$$



Aggregation for phantom nodes: 1D

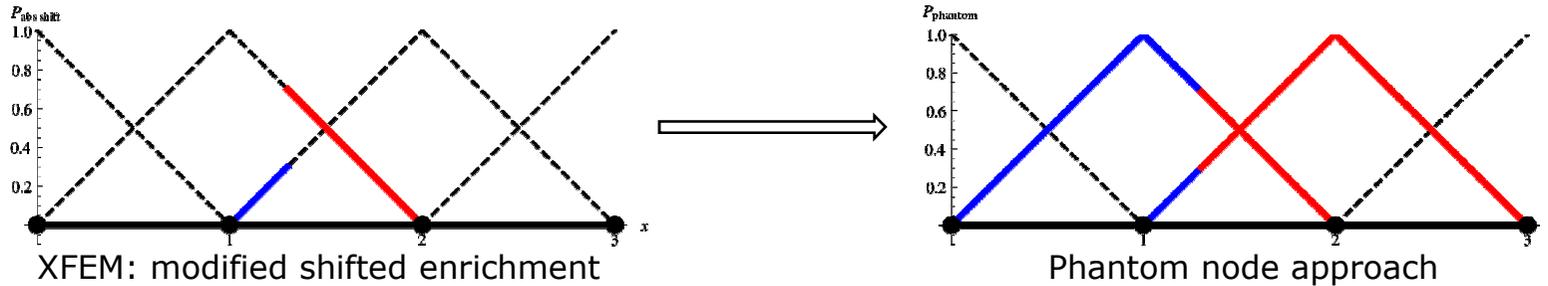


Aggregates seemingly overlap, but are **not** connected on any level!



Transformation

Do XFEM developers have to use the phantom node approach? No!



For each node I with jump DOFs: $\phi_I - \bar{\phi}_I = \phi_\alpha$

$$\bar{\phi}_I = \bar{\phi}_\alpha$$

$$G^T \cdot A \cdot G \cdot G^{-1} \cdot u = G^T \cdot f$$

$$G^T = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & -1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & -1 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{matrix} u_1 \\ u_2 \\ a_3 \\ a_2 \\ u_3 \\ u_4 \end{matrix}$$

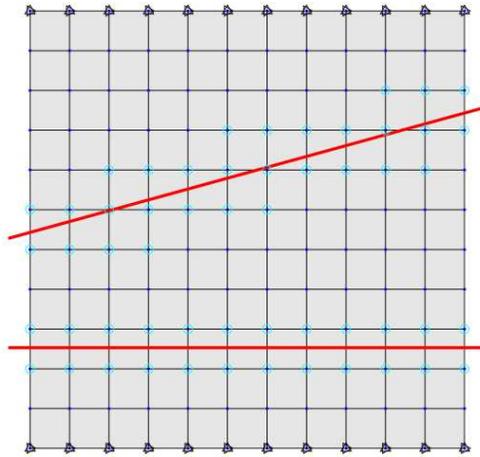
(similar: Menouillard 2008, ...)

G

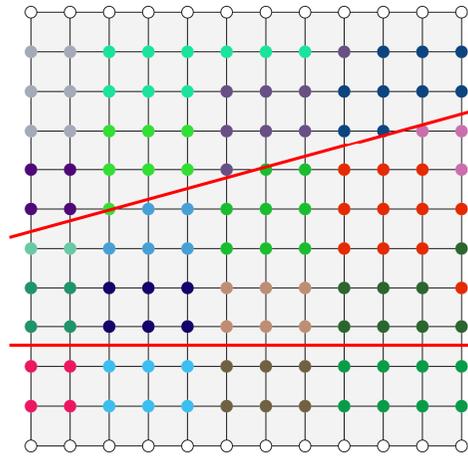
- is extremely sparse,
- is simple to produce,
- transformations can be processor-local, and
- exists for higher order Lagrange Polynomials and multiple dimensions.



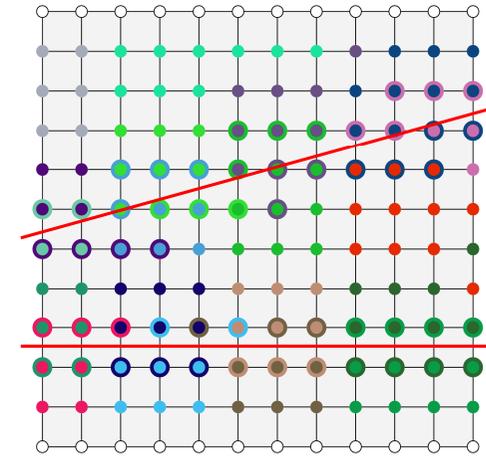
Aggregation for phantom nodes: 2D



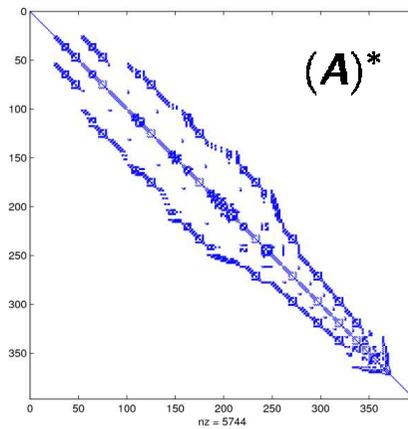
Mesh + BC + Enrichment



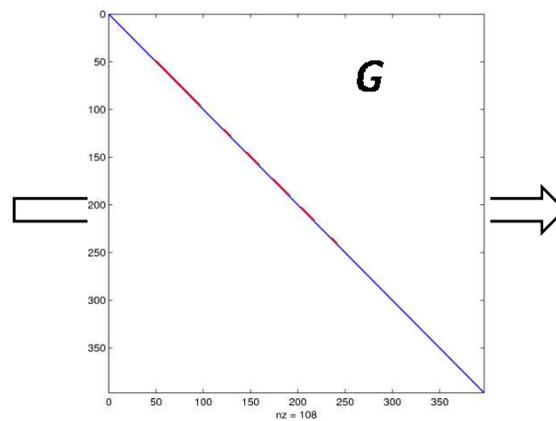
Standard DOFs only



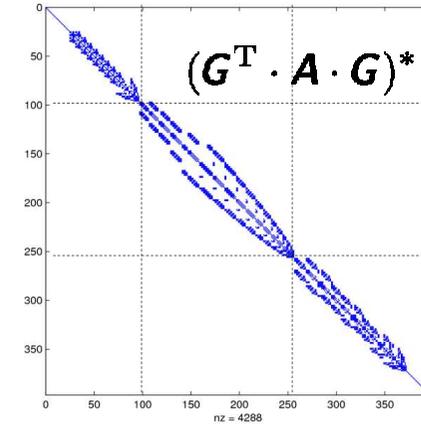
Standard + Phantom DOFs



Modified shifted enrichment



$$G^T \cdot A \cdot G \cdot G^{-1} \cdot u = G^T \cdot f$$



Phantom node approach

()* → sym. rev. Cuthill-McKee permutation for visualization

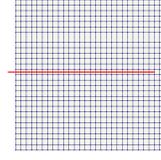
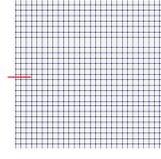
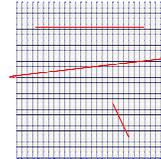
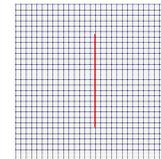
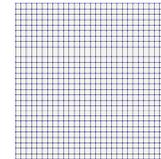


Prelim. results for jump enrichments only

CG preconditioned with AMG

A Shifted enrichment

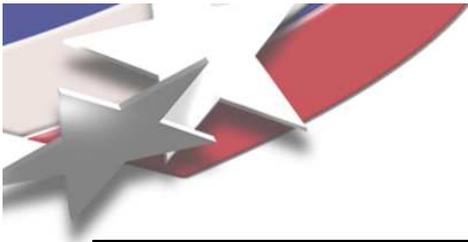
$G^T \cdot A \cdot G$ Phantom node



If one wants to use the standard graph-based aggregation, then using Phantom node setup is crucial!

Case	$n_e \times n_e$	$\alpha_{\text{cond.}}$	n_{iter}			
			A		$G^T \cdot A \cdot G$	
			1L	ML	1L	ML
I	30 × 30	3e+03	32	9	32	9
	60 × 60	1e+04	63	10	63	10
	90 × 90	3e+04	93	11	93	11
	120 × 120	5e+04	123	11	123	11
II	30 × 30	2e+06	59	40	53	12
	60 × 60	1e+06	109	58	104	13
	90 × 90	2e+06	159	65	156	14
	120 × 120	1e+07	-	81	-	15
III	30 × 30	1e+04	46	25	42	11
	60 × 60	5e+04	86	33	83	13
	90 × 90	1e+05	127	40	127	15
	120 × 120	2e+05	170	44	167	15
1a	30 × 30	1e+05	54	16	54	11
	60 × 60	4e+05	106	21	105	14
	90 × 90	1e+06	157	24	157	16
	120 × 120	2e+06	-	26	-	16
1c	30 × 30	2e+07	78	38	76	16
	60 × 60	7e+07	150	53	146	17
	90 × 90	1e+08	-	63	-	18
	120 × 120	2e+08	-	73	-	21

OC: 1.28-1.40



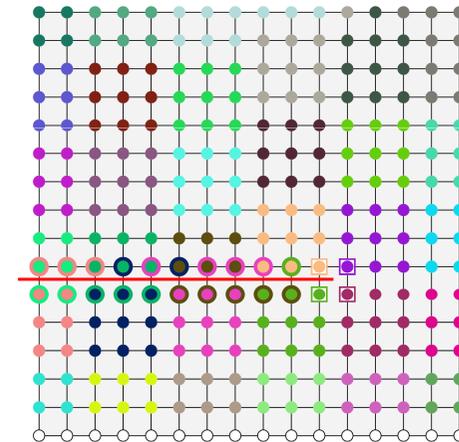
NullSpace for Jump & Tip Enrichments

2D Elasticity problem has 3 Zero Energy Modes (ZEMs):

	1	2	3
d_{xI}	1	0	$-y_I$
d_{yI}	0	1	x_I
		...	

Nullspace for phantom node setup

- Standard DOFs are treated as usual
- Phantom DOFs are treated like Standard DOFs
- *Extra tip DOFs don't contribute to rigid body motion*
 - Put 0 into their respective rows
 - no coarse level contribution in prolongation & restriction
 - smoothing only on finest level (fine scale feature)

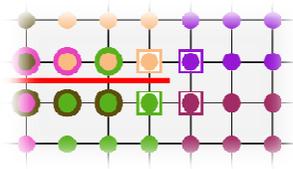


$$+ \sum_{i=1}^{n_f} N_{\hat{f}_i}(\mathbf{x}) \sum_{J=1}^{n_J} \left(F_J(\mathbf{x}) - F_J(\mathbf{x}_{\hat{f}_i}) \right) b_{\hat{f}_i J} \quad F_J(r, \theta) = \left\{ \overbrace{\sqrt{r} \sin\left(\frac{\theta}{2}\right)}^{J=1}, \overbrace{\sqrt{r} \cos\left(\frac{\theta}{2}\right)}^{J=2}, \overbrace{\sqrt{r} \sin\left(\frac{\theta}{2}\right) \sin(\theta)}^{J=3}, \overbrace{\sqrt{r} \cos\left(\frac{\theta}{2}\right) \sin(\theta)}^{J=4} \right\}$$



Smoothing

- Finest Level: Use special tip smoother D^{tip} in addition to standard (Block-) Gauss-Seidel smoothing



Reason for special smoothing:

- dense blocks (40x40 for quad4)
- high condition number

– Tip smoother: direct solve for each small tip block

– Pre-smoother

$$u \leftarrow \text{GaussSeidel}(u, \tilde{A}, b)$$

$$u \leftarrow u + D^{\text{tip}} \cdot (b - \tilde{A} \cdot u)$$

– Post-smoother

$$u \leftarrow u + D^{\text{tip}} \cdot (b - \tilde{A} \cdot u)$$

$$u \leftarrow \text{GaussSeidel}(u, \tilde{A}, b)$$

Pre-Post-smoother symmetry is important

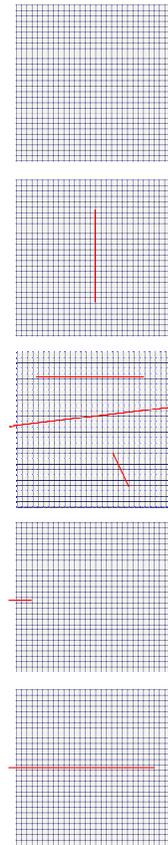
- All coarser levels: standard (Block-) Gauss-Seidel
- Coarsest Level: standard direct solve



Numerical Results for full XFEM system

CG preconditioned with AMG

Special tip smoother is essential to deal with tip enrichments!



Case	$n_e \times n_e$	$\alpha_{\text{cond.}}$	n_{iter}				
			1L	ML	ML, NS	ML, MS	ML, MS, NS
I	30×30	$3e+03$	32	9	9	9	9
	60×60	$1e+04$	63	10	10	10	10
	90×90	$3e+04$	93	11	11	11	11
	120×120	$5e+04$	123	11	11	11	11
II	30×30	$2e+07$	115	84	75	21	18
	60×60	$8e+08$	-	115	97	24	20
	90×90	$8e+09$	-	141	114	27	23
	120×120	$3e+10$	-	-	143	28	23
III	30×30	$5e+07$	143	122	94	24	18
	60×60	$1e+09$	-	180	158	27	20
	90×90	$2e+10$	-	-	-	29	20
	120×120	$3e+10$	-	-	-	37	26
1a	30×30	$6e+05$	66	31	31	16	16
	60×60	$3e+06$	117	31	31	18	18
	90×90	$1e+07$	165	33	33	20	20
	120×120	$2e+07$	-	32	32	19	19
1c	30×30	$1e+08$	86	34	34	21	20
	60×60	$7e+08$	157	35	35	23	23
	90×90	$2e+09$	-	35	35	24	24
	120×120	$3e+09$	-	37	37	26	26

Operator complexity: 1.28-1.40



Concluding Remarks

Standard SA-AMG methods can be used, if proper input is provided!

Key components:

- System matrix must be in phantom-node form
 - Either you already have it, (voids, fluid-structure interaction, ...) , or
 - do a simple transformation $\mathbf{G}^T \cdot \mathbf{A} \cdot \mathbf{G} \cdot \mathbf{G}^{-1} \cdot \mathbf{u} = \mathbf{G}^T \cdot \mathbf{f}$
- Adapt nullspace with zero entries for extra tip DOFs
- Two-step smoothing on finest level

Future Directions

- What happens to tiny element fractions (conditioning)?
- 3d implementation